

6238a

U. S. COAST & GEODETIC SURVEY
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6238a

Form 504
Rev. Dec. 1933
DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
R. S. PATTON, DIRECTOR

DESCRIPTIVE REPORT
GRAPHIC CONTROL
~~Topographic~~ Sheet No. _____ G
~~Hydrographic~~

State _____ Virginia _____

LOCALITY
Chincoteague Island
~~Assateague Inlet~~
Assateague Inlet & Vicinity
~~Beach Hole Creek~~

~~Little Bay~~

193 4

CHIEF OF PARTY
H. A. Seran

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY

U. S. COAST & GEODETIC SURVEY
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TOPOGRAPHIC TITLE SHEET

GRAPHIC CONTROL SHEET

The Topographic Sheet should be accompanied by this form, filled in as completely as possible, when the sheet is forwarded to the Office.

Field No. G

REGISTER NO. **6238a**

State VIRGINIA

General locality CHINCOTEAGUE ^{Island} INLET AND VICINITY

Locality ASSATEAGUE INLET -- ~~PINKY ISLAND~~ AND VICINITY

Scale 1:10,000 Date of survey Oct. 22-24, 19 34

Vessel Sub-party Ship OCEANOGRAPHER

Chief of party H. A. Seran

Surveyed by J. E. Waugh -- C. R. Dodson

Inked by F. J. Kish, J. E. Waugh, C. R. Dodson

Heights in feet above ~~XXXXXXXXXXXX~~ ground ~~XXXX~~ tops of trees

Contour ~~XXXX~~ approximate contour ~~XXXX~~ from line interval ~~XXXX~~ feet

Instructions dated April 27, 1933 -- June 19, 19 34

Remarks: This sheet is for the control of hydrographic survey.

DESCRIPTIVE REPORT

to accompany

GRAPHIC CONTROL SHEET (Field Letter G.)

CHINCOTEAGUE INLET AND VICINITY

Sup-party Ship OCEANOGRAPHER

H. A. Seran, Chief of Party

PROJECT NO. H.T. 142

The descriptive report for Topographic Sheet (field letter G) which covers the plane table control for hydrography in Assateague Inlet, Little Bay and Deep Hole Creek.

INSTRUCTIONS:

The topography on Sheet G is a part of Project No. H.T. 142. The instructions for this part of the project are dated June 19, 1934.

LIMITS AND SCALE:

The scale of this sheet is 1:10,000. It covers that area between Latitudes $37^{\circ}-53.9$ and $37^{\circ}-57.00$ and Longitude $75^{\circ}-18.8$ and $75^{\circ}-24.0$.

CONTROL AND SURVEY METHODS:

The control consisted of two triangulation stations of third order accuracy, and three, three point fixes obtained with the theodolite. The location of triangulation station Assateague Light House, 1902,32,33, is Lat $37^{\circ}-54'$ $+1227.0$ m and Long. $75^{\circ}-21'$ $+561.6$ m.

The usual plane table survey methods were used. The plane table positions were obtained by resection and three point problem methods. There were no traverses.

This sheet was for the location of signals for hydrographic purposes only. The shore line and detail topography was furnished the party by the office.

MARSHES: The marshes in this area are large and are covered at high water. The soil is soft and boggy and is covered by marsh grass.

MAGNETIC MERIDANS:

The magnetic meridan as indicated on the sheet was determined at three point fix No. Four. The declinatoire was not checked in the field because the magnetic declination was not known and no instruments were on hand to make the necessary observations.

AIDS TO NAVIGATION:

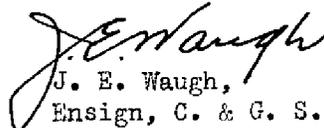
None.

RECOVERABLE TOPOGRAPHIC STATIONS:

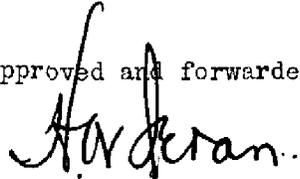
The description of three recoverable topographic stations on this sheet are being submitted on form 524.

LANDMARKS: There is one object on this sheet that can be used as a landmark. Form No. 567 is attached.

Respectfully submitted,


J. E. Waugh,
Ensign, C. & G. S.

Approved and forwarded:


H. A. Seran, Comdr., C. & G. S.

PLANE TABLE POSITION:

1. Gable, east, Derrickson-Hill Oyster House (⊙Whit)
2. Gable, southwest, small house on Myers Flat (⊙Sup)
3. Gable, east, Reid's Clam House (⊙Set)

Station: Ken

State: Maryland

Chief of party: C. V. H.

Date: 1917

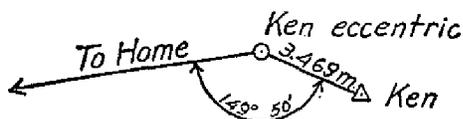
Computed by: O. P. S.

Observer: C. V. H.

Instrument: No. 168

Checked by: W. F. R.

OBSERVED STATION	Observed direction			Eccentric reduction	Sea level reduction	Corrected direction with zero initial			Adjusted direction
	°	'	"			°	'	"	
Chey	0	00	00.00	-	7.31	0	00	00.00	
Tank west of Δ Dulce	29	03	37.0	-1	09.8	29	02	34.5	
Ken (center), 3.469 meters	176	42							
Forest Glen standpipe	313	24	53.0	+3	01.2	313	28	01.5	
Home	326	31	30.21	+	31.93	326	32	09.45	
Bureau of Standards, wireless pole	352	17	20.8	+	5.7	352	17	33.8	
Reno	357	23	43.63	-	1.16	357	28	54.78	
Reference mark, 16.32 m	358	31	20						



This form, with the first three and fifth columns properly filled out and checked, must be furnished by field parties. To be acceptable it must contain every direction observed at the station.

It should be used for observations with both repeating and direction theodolites.

The directions at only one station should be placed on a page.

If a repeating theodolite is used, do not abstract the angles in tertiary triangulation. The local adjustment corrections (to close horizon only) are to be written in the Horizontal Angle Record, and the List of Directions is to be made from that record directly.

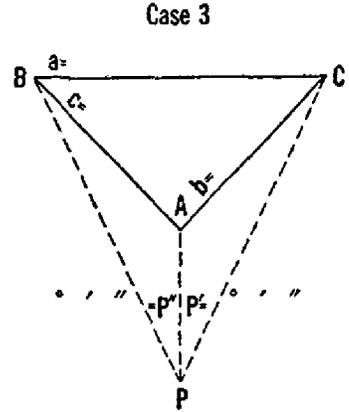
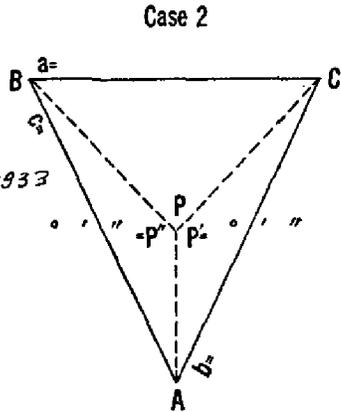
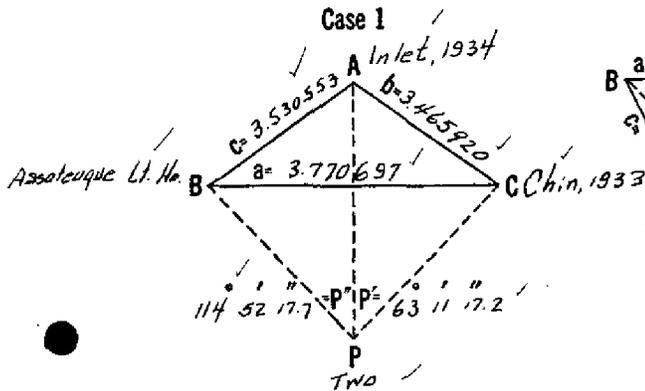
Choose as an initial for Form 24A some station involved in the local adjustment, and preferably one which has been used as an initial for a round of directions on objects not in the main scheme. Use but one initial at a station. Call the direction of the initial 0° 00' 00." 00, and by applying the corrected angles to this, fill in opposite each station its direction reckoned clockwise around the whole circumference regardless of the direction of graduation of the instrument. The clockwise reckoning is necessary for uniformity and to make the directions comparable with azimuths.

If a station has been occupied eccentrically, reduce to the center and enter in this form, in ink, the resulting corrections to the observed directions in the column provided for them. If an eccentric reduction is necessary, but not made in the field, leave the column blank. If the station was occupied centrally, and no eccentric reduction is required, put dashes in the column to show that no corrections are necessary.

Directions in the main scheme should be entered to hundredths of seconds in first-order triangulation; otherwise to tenths only. Points observed upon but once, direct and reverse, should be carried to tenths in first-order and second-order triangulation, and to even seconds only in third-order triangulation. In general, but two uncertain figures should be given.

It is recommended that the following simple plan of observing be used with a repeating instrument: Measure each single angle in the scheme at each station and the outside angle necessary to close the horizon. Measure no sum angles. Follow each measurement of every angle immediately by a measurement of its supplement. Six repetitions are to constitute a measurement. The local adjustment will consist simply of the distribution of the error of closure of the horizon.

Fourth Order
COMPUTATION OF THREE-POINT PROBLEM



Cases 1 and 2		Case 3			
P'	63° - 11' - 17.2 ✓	P'			
P''	114 - 52 - 17.7 ✓	P''			
A	137 - 55 - 27.3 ✓				
		Sum			
Sum	315 - 59 - 02.2 ✓	A			
1/2 Sum	157 - 59 - 31.1 ✓				
		A - sum			
S = 180° - 1/2 sum =	22 - 00 - 28.9 ✓	S = 1/2 (A - sum) =			
Log c =	3.530553 ✓				
Log sin P' =	9.950604 ✓				
Colog b =	6.534080 ✓				
Colog sin P'' =	0.042272 ✓				
Sum = log tan Z =	0.057509 ✓				
Z =	48° - 46' - 57.0 ✓				
Z + 45° =	93 - 46 - 57.0 ✓				
Log cot (Z + 45°) =	8.820288 n ✓				
Log tan S =	9.606585 ✓				
Sum = log tan ε =	8.426873 ✓	(sign n)			
ε	1° - 31' - 50.6 ✓				
S	22 - 00 - 28.9 ✓				
(Tan ε +)		(Tan ε -)			
S + ε = angle ABP	20° - 28' - 38.3 ✓	S - ε = angle ABP			
S - ε = angle ACP	23° - 32' - 19.5 ✓	S + ε = angle ACP			
BPA	114° - 52' - 17.7 ✓	APC	63° - 11' - 17.2 ✓	PCB	00° - 51' - 55.1 ✓
ABP	20 - 28 - 38.3 ✓	PCA	23 - 32 - 19.5 ✓	CBP	01 - 04 - 30.0 ✓
PAB	44 - 39 - 04.0 ✓	CAP	93 - 16 - 23.3 ✓	BPC	178 - 03 - 34.9 ✓

(For explanation of this form see Special Publication No. 138, pages 191 and 192, or Special Publication No. 145, pages 98-100)

Comp 8200
F.S.J.
Copy 8200
357

Fourth Order

COMPUTATION OF TRIANGLES

State: VIRGINIA

11-9121

NO.	STATION	OBSERVED ANGLE	CORR'N	SPHER'L ANGLE	SPHER'L EXCESS	PLANE ANGLE AND DISTANCE	LOGARITHM
	2-3						3.465920'
	1 No. Two	63°-11'-17.2'					0.049396'
	2 Inlet, 1934	93-16-23.3'					9.999291'
	3 Chin, 1933	23-32-19.5'					9.601375'
	1-3						3.514607'
	1-2						3.116691'
	2-3						3.530553'
	1 No. Two	114°-52'-17.7'					0.042272'
	2 Assateague Lt. Ho.	20-28-38.3'					9.543865'
	3 Inlet, 1934	44-39-04.0'					9.846824'
	1-3						3.116690'
	1-2						3.419649'
	2-3						
	1						
	2						
	3						
	1-3						
	1-2						
	2-3						
	1						
	2						
	3						
	1-3						
	1-2						

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Comp by J.S.M.
✓ by J.S.M.
Copy by J.S.M.
" " J.S.M.

Fourth Order
POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY
FORM 37
Ed. April, 1923

		" ' " "		" ' " "		" ' " "		" ' " "		" ' " "		" ' " "	
		63		63		63		63		63		63	
		FIRST ANGLE OF TRIANGLE		FIRST ANGLE OF TRIANGLE		FIRST ANGLE OF TRIANGLE		FIRST ANGLE OF TRIANGLE		FIRST ANGLE OF TRIANGLE		FIRST ANGLE OF TRIANGLE	
α	2 Inlet, 1934 to 3 Chin, 1933	99	04	27.0		3 Chin, 1933 to 2 Inlet, 1934	279	03	15.2				
$2^{\text{d}} \angle$	Chin, 1933 & No. Two	+ 93	16	23.3		Inlet, 1934 & No. Two	- 23	32	19.5				
α	2 Inlet, 1934 to 1 No. Two	192	30	51.1		3 Chin, 1933 to 1 No. Two	255	30	55.7				
$\Delta \alpha$		+ 00	07.0				+ 01	01	19.6				
		180	00	00.0			180	00	00.0				
α'	1 No. Two to 2 Inlet, 1934	12	20	58.1		1 No. Two to 3 Chin, 1933	75	32	15.3				
" ' " " " ' " " " ' " " " " ' " "													
ϕ	37 53 39.88 2 Inlet, 1934	λ	75 23 19.47			37 53 54.82 3 Chin, 1933	λ	75 25 17.64					
$\Delta \phi$	+ 00 41.45	$\Delta \lambda$	- 00 11.45				$\Delta \lambda$	- 02 09.62					
ϕ'	37 54 21.33 1 No. Two	λ'	75 23 08.02				λ'	75 23 08.02					
" ' " " " ' " " " ' " " " " ' " "													
		Values in seconds		Values in seconds		Values in seconds		Values in seconds		Values in seconds		Values in seconds	
s	3.116 691	$\frac{1}{2}(\phi+\phi')$	37 54 00.6	s	3.514 607	$\frac{1}{2}(\phi+\phi')$	37 54 08.1	Logarithms	37 54 08.1	s	3.514 607	Logarithms	37 54 08.1
$\text{Cos } \alpha$	9.989 836	s	3.116 691	$\text{Cos } \alpha$	9.398 146	s	9.985 972	s	9.985 972	s	3.514 607	s	3.514 607
B	8.511 011	$\text{Sin } \alpha$	8.509 171	B	8.511 010	$\text{Sin } \alpha$	8.509 171	$\text{Sin } \alpha$	8.509 171	$\text{Sin } \alpha$	8.509 171	$\text{Sin } \alpha$	8.509 171
h	1.617 538	$\text{Sec } \phi'$	0.102 912	h	1.423 763	$\text{Sec } \phi'$	0.102 912	$\text{Sec } \phi'$	0.102 912	$\text{Sec } \phi'$	0.102 912	$\text{Sec } \phi'$	0.102 912
s^2	6.233 4	$\Delta \lambda$	1.058 865	s^2	7.029 2	$\Delta \lambda$	2.112 662	$\Delta \lambda$	2.112 662	$\Delta \lambda$	2.112 662	$\Delta \lambda$	2.112 662
$\text{Sin}^2 \alpha$	8.660 2	$\text{Sin } \frac{1}{2}(\phi+\phi')$	9.788 372	$\text{Sin}^2 \alpha$	9.971 9	$\text{Sin } \frac{1}{2}(\phi+\phi')$	9.788 392	$\text{Sin } \frac{1}{2}(\phi+\phi')$	9.788 392	$\text{Sin } \frac{1}{2}(\phi+\phi')$	9.788 392	$\text{Sin } \frac{1}{2}(\phi+\phi')$	9.788 392
C	1.295 9	$-\Delta \alpha$	0.847 237	C	1.296 0	$-\Delta \alpha$	1.901 054	$\Delta \alpha$	1.901 054	$-\Delta \alpha$	1.901 054	$-\Delta \alpha$	1.901 054
	6.189 5	2^{d} term	+ 0.02		8.29 71	2^{d} term	+ 0.02	2^{d} term	+ 0.02	2^{d} term	+ 0.02	2^{d} term	+ 0.02
h^2		3^{d} term	+ 0.02			3^{d} term	+ 0.02	3^{d} term	+ 0.02	3^{d} term	+ 0.02	3^{d} term	+ 0.02
D		$-\Delta \phi$	- 41.45			$-\Delta \phi$	- 26.51	$-\Delta \phi$	- 26.51	$-\Delta \phi$	- 26.51	$-\Delta \phi$	- 26.51

*Comp by Jen
Copy by Jen*

Station: Ken

State: Maryland

Chief of party: C. V. H.

Date: 1917

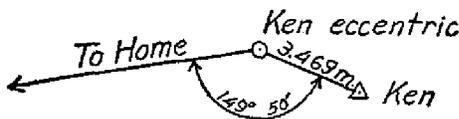
Computed by: O. P. S.

Observer: C. V. H.

Instrument: No. 168

Checked by: W. F. R.

OBSERVED STATION	Observed direction			Eccentric reduction	Sea level reduction	Corrected direction with zero initial			Adjusted direction
	°	'	"			°	'	"	
Chevy	0	00	00.00	-	7.31	0	00	00.00	
Tank west of Δ Dulce	29	03	37.0	-1	09.8	29	02	34.5	
Ken (center), 3.469 meters	176	42							
Forest Glen standpipe	313	24	53.0	+3	01.2	313	28	01.5	
Home	326	31	30.21	+	31.93	326	32	09.45	
Bureau of Standards, wireless pole ..	352	17	20.8	+	5.7	352	17	33.8	
Reno	357	28	48.63	-	1.16	357	28	54.78	
Reference mark, 16.32 m	358	31	20						



This form, with the first three and fifth columns properly filled out and checked, must be furnished by field parties. To be acceptable it must contain every direction observed at the station.

It should be used for observations with both repeating and direction theodolites.

The directions at only one station should be placed on a page.

If a repeating theodolite is used, do not abstract the angles in tertiary triangulation. The local adjustment corrections (to close horizon only) are to be written in the Horizontal Angle Record, and the List of Directions is to be made from that record directly.

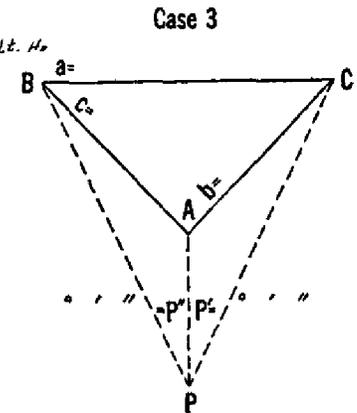
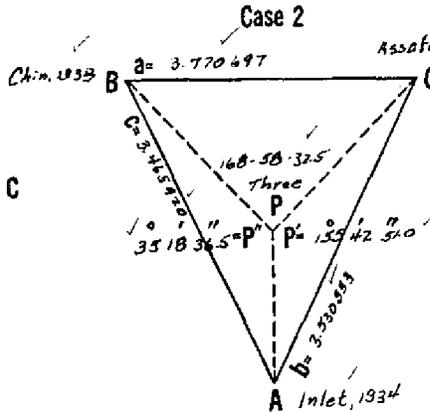
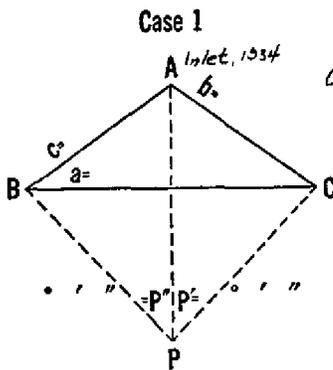
Choose as an initial for Form 24A some station involved in the local adjustment, and preferably one which has been used as an initial for a round of directions on objects not in the main scheme. Use but one initial at a station. Call the direction of the initial 0° 00' 00." 00, and by applying the corrected angles to this, fill in opposite each station its direction reckoned clockwise around the whole circumference regardless of the direction of graduation of the instrument. The clockwise reckoning is necessary for uniformity and to make the directions comparable with azimuths.

If a station has been occupied eccentrically, reduce to the center and enter in this form, in ink, the resulting corrections to the observed directions in the column provided for them. If an eccentric reduction is necessary, but not made in the field, leave the column blank. If the station was occupied centrally, and no eccentric reduction is required, put dashes in the column to show that no corrections are necessary.

Directions in the main scheme should be entered to hundredths of seconds in first-order triangulation; otherwise to tenths only. Points observed upon but once, direct and reverse, should be carried to tenths in first-order and second-order triangulation, and to even seconds only in third-order triangulation. In general, but two uncertain figures should be given.

It is recommended that the following simple plan of observing be used with a repeating instrument: Measure each single angle in the scheme at each station and the outside angle necessary to close the horizon. Measure no sum angles. Follow each measurement of every angle immediately by a measurement of its supplement. Six repetitions are to constitute a measurement. The local adjustment will consist simply of the distribution of the error of closure of the horizon.

Fourth Order
COMPUTATION OF THREE-POINT PROBLEM



Cases 1 and 2		Case 3			
P'	155-42-51.0 ✓	P'			
P''	35-18-36.5 ✓	P''			
A	137-55-27.3 ✓				
Sum	328-56-54.8 ✓	Sum			
1/2 Sum	164-28-27.4 ✓	A			
S = 180° - 1/2 sum =	15-31-32.6 ✓	A - sum			
		S = 1/2 (A - sum) =			
Log c =	3.465920 ✓				
Log sin P' =	9.614147 ✓				
Colog b =	6.469447 ✓				
Colog sin P'' =	0.230071 ✓				
Sum = log tan Z =	9.787585 ✓				
Z =	31° 30' - 56.2 ✓				
Z + 45° =	76-30-56.2 ✓				
Log cot (Z + 45°) =	9.379832 ✓				
Log tan S =	9.443745 ✓				
Sum = log tan ε =	8.823577 ✓	(sign +)			
ε =	3° 48' - 40.2 ✓				
S =	15° 31' - 32.6 ✓				
(Tan ε +)		(Tan ε -)			
S + ε = angle ABP	19° 20' - 12.8 ✓	S - ε = angle ABP			
S - ε = angle ACP	11 - 42 - 52.4 ✓	S + ε = angle ACP			
BPA	35-18-36.5 ✓	APC	155-42-51.0 ✓	PCB	7° 41' - 15.9 ✓
ABP	19-20-12.8 ✓	PCA	11-42-52.4 ✓	CBP	3-20-11.6 ✓
PAB	125-21-10.7 ✓	CAP	12-34-16.6 ✓	BPC	168-58-32.5 ✓

(For explanation of this form see Special Publication No. 138, pages 191 and 192, or Special Publication No. 145, pages 98-100)

*Comp by J.E.W.
Ref 7.5.T.
copy by J.E.W.
7.5.T.*

Fourth Order

COMPUTATION OF TRIANGLES

State: VIRGINIA

11-9121

NO.	STATION	OBSERVED ANGLE	CORR'N	SPHERE'S ANGLE	SPHERE'S EXCESS	PLANE ANGLE AND DISTANCE	LOGARITHM
	2-3						3.530553 /
1	No. Three	155°-42'-51.0 /					0.385853 /
2	Assateague Lt. Ho.	11-42-52.4 /					9.307573 /
3	Inlet, 1934	12-34-16.6 /					9.337767 /
	1-3						3.223979 /
	1-2						3.254173 /
	2-3						3.465920 /
1	No. Three	35°-18'-36.5 /					0.238071 /
2	Inlet, 1934	125-21-10.7 /					9.911479 /
3	Chin, 1933	19-20-12.8 /					9.519988 /
	1-3						3.615470 /
	1-2						3.223979 /
	2-3						
	1						
	2						
	3						
	1-3						
	1-2						
	2-3						
	1						
	2						
	3						
	1-3						
	1-2						

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" " " F.S.J.

6238b

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APR 2 1935

Acc. No. _____

Form 504
Rev. Dec. 1933
DEPARTMENT OF COMMERCE
U.S. COAST AND GEODETIC SURVEY
R. S. PATTON, DIRECTOR

DESCRIPTIVE REPORT

GRAPHIC CONTROL

~~Topographic~~
~~Hydrographic~~

Sheet No. H

State VIRGINIA

LOCALITY

CHINCOTEAGUE ~~Island~~

ASSATEAGUE BAY & Vicinity

~~DIG BAY~~

1934

CHIEF OF PARTY

H. A. Seran

6238b

DESCRIPTIVE REPORT

to accompany

GRAPHIC CONTROL SHEET (Field letter H)

CHINCOTEAGUE INLET AND VICINITY

Subparty Ship OCEANOGRAPHER

H. A. Seran, Chief of Party

PROJECT NO. H.T. 142

The descriptive report for Topographic Sheet (field letter H) which covers the plane table control for hydrography in Assateague Bay, Big Bay and Chincoteague Bay is herewith submitted.

INSTRUCTIONS:

The topography on Sheet H is part of Project No. H.T. 142. The instructions for this part of the project are dated June 19, 1934.

LIMITS AND SCALE:

The scale of this sheet is 1: 10,000. It covers that area between Latitudes $37^{\circ}-56'.8$ and $37^{\circ}-59'.8$ and Longitudes $75^{\circ}-17'.6$ and $75^{\circ}-22'.7$.

CONTROL AND SURVEY METHODS:

The control consisted of five triangulation stations of third order accuracy and three, three point fixes obtained with the theodolite. The location of triangulation station Blake is Latitude $37^{\circ}-57'+260.2$ m, Longitude $75^{\circ}-21'+623.0$ m.

The usual plane table survey methods were used. The plane table positions were obtained by resection and three point problem methods. There were no traverses. The signals in Big Bay and Assateague Bay were located from triangulation station Wildcat and three point fixes Nos. Four, Five and Six before the triangulation on the west side of Chincoteague Island was executed. After this triangulation was completed it was used for control in locating the signals on the west side of Chincoteague Island. The location of the signals on the east side of the Island were checked at the same time and the positions were found to check satisfactorily.

This sheet was for the location of signals for hydrographic purposes only. The shore line and detail topography was furnished the party by the office.

MARSHES:

The marshes in this area are large and are covered at high water. The soil is soft and boggy and is covered by marsh grass.

MAGNETIC MERIDANS:

The magnetic meridan as indicated on the sheet was determined at triangulation station Blake, 1934. The declinoaire was not checked in the field because the magnetic declination was not known and no instruments were on hand to make the necessary observations.

AIDS TO NAVIGATION:

Form No. 567 is attached for the aids to navigation on this sheet. This beacon marks the best water between Franklin City and Chincoteague Island.

RECOVERABLE TOPOGRAPHIC STATIONS:

The description of two recoverable topographic stations on this sheet are being submitted on form 524.

LANDMARKS: There are no land marks on this sheet.

Respectfully submitted,

J. E. Waugh
J. E. Waugh,
Ensign, C. & G. S.

Approved and forwarded:

H. A. Seran
H. A. Seran, Comdr. C. & G. S.,
Commanding Ship OCEANOGRAPHER.

PLANE TABLE POSITIONS:

1. Gable, south, Lone House, east side Assateague Bay. (⊙ Tess)
2. Chimney, Dr. Lekite's Hunting Lodge. (⊙ Fill)

Duplicate

DEPARTMENT OF COMMERCE
U. S. COAST AND GEODETIC SURVEY

LANDMARKS FOR CHARTS

Norfolk, Virginia

DIRECTOR, U. S. COAST AND GEODETIC SURVEY:

_____, 193

The following determined objects are prominent, can be readily distinguished from seaward from the description given below, and should be charted.

H. A. Seran.

AIDS TO NAVIGATION

H. A. Seran

Chief of Party.

DESCRIPTION	POSITION					METHOD OF DETERMINATION	CHARTS AFFECTED	
	LATITUDE			LONGITUDE				DATUM
	°	'	D. M. METERS	°	'			
BEACON; FLR. red no.								
four (Δ Red Beacon No.								
Four, 1934)	37 - 58		1125.1 ✓	75 - 22		NA 1927	New Tri- angulation No. 1220 ✓	

This position was copied checked against original. J. Erbaugh

A list of objects carefully selected because of their value as landmarks as determined from seaward together with individual descriptions, must be furnished in a special report on this form, and a copy of such report must be attached by the Chief of Party to his descriptive report.
The selection, determination, and description of these points are an important factor in the value of the chart. Landmarks selected at appropriate intervals can be clearly charted. However, when none is outstanding, a group of two or three objects may by their interrelationship provide positive identification. A group so selected should be indicated.
The description of each object should be short, but such as will clearly identify it; for example, a standpipe, elevated tank, gas tank, church spire, tall stack, red chimney, radio mast, etc. Assign numerals to landmarks to indicate: (1) offshore, (2) inshore, (3) harbor, 1, 2, 3 would be a mark useful on all charts. Generally, flagstaffs and like objects are not sufficiently permanent to chart.

Station: Ken

State: Maryland

Chief of party: C. V. H.

Date: 1917

Computed by: O. P. S.

Observer: C. V. H.

Instrument: No. 168

Checked by: W. F. R.

OBSERVED STATION	Observed direction			Eccentric reduction	Sea level reduction	Corrected direction with zero initial			Adjusted direction
	°	'	"			°	'	"	
Chevy.....	0	00	00.00	-	7.31	0	00	00.00	
Tank west of Δ Dulce.....	29	03	37.0	-1	09.8	29	02	34.5	
Ken (center), 3.469 meters.....	176	42							
Forest Glen standpipe.....	313	24	53.0	+3	01.2	313	28	01.5	
Home.....	326	31	30.21	+	31.93	326	32	09.45	
Bureau of Standards, wireless pole.....	352	17	20.8	+	5.7	352	17	33.8	
Reno.....	357	28	48.63	-	1.16	357	28	54.78	
Reference mark, 16.32 m.....	358	31	20						

Ken eccentric
3.469m
149° 56'

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Choose as an initial for Form 24A some station involved in the local adjustment, and preferably one which has been used as an initial for a round of directions on objects not in the main scheme. Use but one initial at a station. Call the direction of the initial 0° 00' 00." 00, and by applying the corrected angles to this, fill in opposite each station its direction reckoned *clockwise* around the whole circumference regardless of the direction of graduation of the instrument. The clockwise reckoning is necessary for uniformity and to make the directions comparable with azimuths.

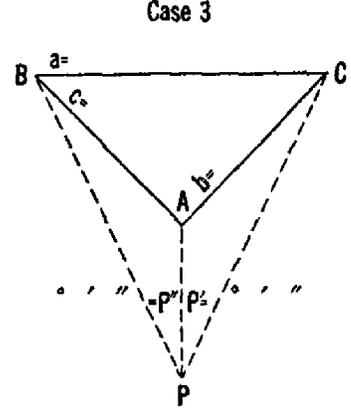
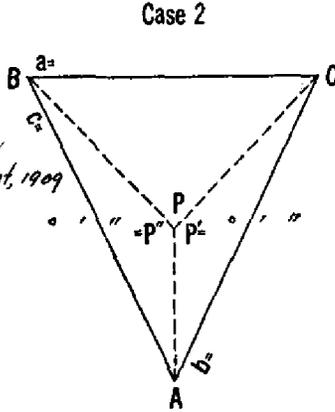
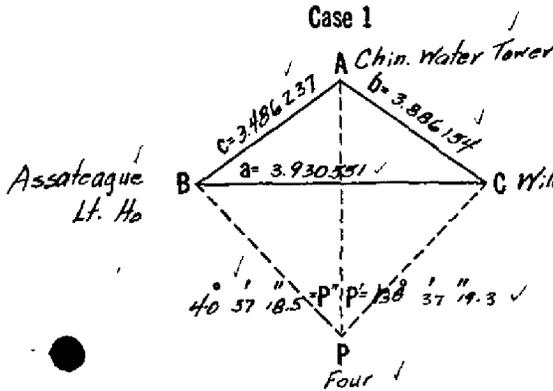
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Fourth Order

COMPUTATION OF THREE-POINT PROBLEM



Cases 1 and 2		Case 3			
P'	138° 37' 19.3 ✓	P'			
P''	40° 57' 18.5 ✓	P''			
A	94° 55' 27.3 ✓				
Sum	274° 30' 05.1 ✓	Sum			
1/2 Sum	137° 15' 02.6 ✓	A			
S = 180° - 1/2 sum =	42° 44' 57.4 ✓	A - sum			
		S = 1/2 (A - sum) =			
Log c =	3.486 237 ✓				
Log sin P' =	9.820 217 ✓				
Colog b =	0.183 449 ✓				
Colog sin P'' =	6.113 846 ✓				
Sum = log tan Z =	9.603 749 ✓				
Z =	21° 52' 42.1 ✓				
Z + 45° =	66° 52' 42.1 ✓				
Log cot (Z + 45°) =	9.630 410 ✓				
Log tan S =	9.965 844 ✓				
Sum = log tan ε =	9.596 254 ✓ (sign +)				
ε	21° 32' 18.8 ✓				
S	42° 44' 57.4 ✓				
(Tan ε +)		(Tan ε -)			
S + ε = angle ABP	64° 17' 16.2 ✓	S - ε = angle ABP			
S - ε = angle ACP	21° 12' 38.6 ✓	S + ε = angle ACP			
BPA	40° 57' 18.5 ✓	APC	138° 37' 19.3 ✓	PCB	00° 13' 23.8 ✓
ABP	64° 17' 16.2 ✓	PCA	21° 12' 38.6 ✓	CBP	00° 11' 58.3 ✓
PAB	74° 45' 25.3 ✓	CAP	20° 10' 02.1 ✓	BPC	179° 34' 37.8 ✓

(For explanation of this form see Special Publication No. 138, pages 191 and 192, or Special Publication No. 145, pages 98-100)

Copied by J.S.T.
✓ by J.S.T.
Copied by J.S.T.

Fourth Order

COMPUTATION OF TRIANGLES

State: VIRGINIA

11-9121

NO.	STATION	OBSERVED ANGLE	CORR'N	SPHER'L ANGLE	SPHER'L EXCESS	PLANE ANGLE AND DISTANCE	LOGARITHM
	2-3						3.4862371
	1 No. Four	40° 57' 18.5"					0.1834491
	2 Assateague Lt. Ho.	64-17-16.2'					9.9547181
	3 Chin. Water Tower	74-45-25.3'					9.9844461
	1-3						3.6244041
	1-2						3.6541321
	2-3						3.8861541
	1 No. Four	138° 37' 19.3"					0.1797831
	2 Chin. Water Tower	20-10-02.1'					9.9375191
	3 Wildcat, 1909	21-12-38.6'					9.5584681
	1-3						3.6034561
	1-2						3.6244051
	2-3						
	1						
	2						
	3						
	1-3						
	1-2						
	2-3						
	1						
	2						
	3						
	1-3						
	1-2						
							Comp by MBM
							✓ by F.S.T.
							Copy by J.S.J.
							" " " F.S.J.

Do not write in this margin

POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

		FIRST ANGLE OF TRIANGLE				SECOND ANGLE OF TRIANGLE				THIRD ANGLE OF TRIANGLE						
		0	1	2	3	0	1	2	3	0	1	2	3			
a	2 Assateague Lt. Ho. to 3 Chin. Water Tower	141	57	14	6'	321	56	271	-	37	56	24	5			
3rd	Chin. Water Tower & No. Four	+	64	17	16.2'	-	74	45	25.3'							
a	2 Assateague Lt. Ho. to 1 No. Four	206	14	30	8	247	11	01.8								
Δα		+	00	58	2	+	01	37	7							
		180	00	00	0.0	180	00	00	00.0							
a'	1 No. Four to 2 Assateague Lt. Ho.	26	25	21	0	67	12	39.5								
0	"	40	57	18	5'											
φ	37	54	39	80	2 Assateague Lt. Ho.	37	55	58	04	3 Chin. Water Tower	37	56	22	40	31	
Δφ	+	02	11	18		+	00	52	94		+	00	02	38	98	
φ'	37	56	50	98	1 No. Four	37	56	50	98	1 No. Four	37	56	20	01	33	
s	3.654132	Values in seconds				37	55	45	4	37	56	24	5	Values in seconds		
Cos α	9.952761	(278.2)				Logarithms	37	55	45	4	Logarithms	37	56	24	5	
B	8.511009	1st term	"	"	"	s	3.624404	Values in seconds				Logarithms	37	56	24	5
h	2.117902	1st term	-131.19	"	"	h	1.723990	1st term	-52.97	"	"	"	3.624404	Values in seconds		
s²	7.3083	A'	8.509171	(432.7)				Sin α	9.964619	Values in seconds		Logarithms	37	56	24	5
Sin² α	9.2912	Sec φ'	0.103157					Sec φ'	0.103157	Values in seconds		Logarithms	37	56	24	5
C	1.2961	Δλ	1.912041					Δλ	2.201351	Values in seconds		Logarithms	37	56	24	5
	7.8956	2d term	+ 0.01					Sin ½(φ+φ')	9.788761	Values in seconds		Logarithms	37	56	24	5
h²		3d term	+					Δα	1.990112	Values in seconds		Logarithms	37	56	24	5
D		-Δφ	-131.18					-Δα	-92.7	Values in seconds		Logarithms	37	56	24	5

11-5532
COMPUTED BY M.B.M.
CHECKED BY J.E.M.

Station: Ken

State: Maryland

Chief of party: C. V. H.

Date: 1917

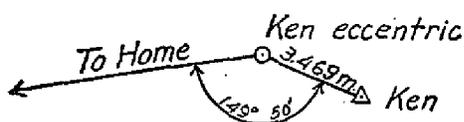
Computed by: O. P. S.

Observer: C. V. H.

Instrument: No. 168

Checked by: W. F. R.

OBSERVED STATION	Observed direction			Eccentric reduction		Sea level reduction	Corrected direction with zero initial			Adjusted direction	
	°	'	"	'	"		°	'	"	'	"
Chevy	0	00	00.00	-	7.31		0	00	00.00		
Tank west of Δ Dulce	29	03	37.0	-1	09.8		29	02	34.5		
Ken (center), 3.469 meters	176	42									
Forest Glen standpipe	313	24	53.0	+3	01.2		313	28	01.5		
Home	326	31	30.21	+	31.93		326	32	09.45		
Bureau of Standards, wireless pole	352	17	20.8	+	5.7		352	17	33.8		
Reno	357	28	48.63	-	1.16		357	28	54.78		
Reference mark, 16.32 m	358	31	20								



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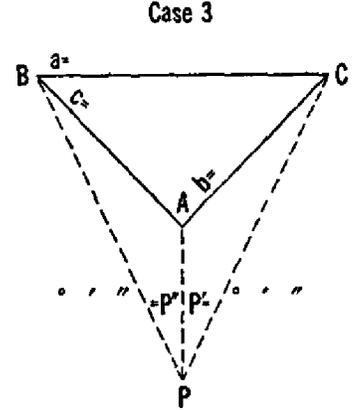
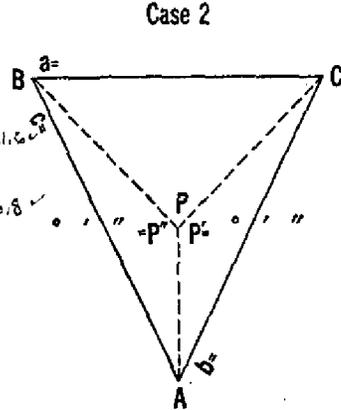
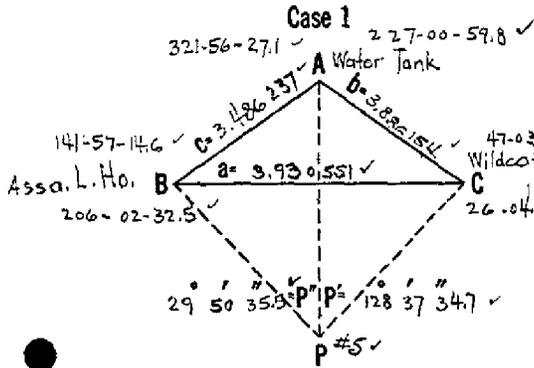
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Fourth Order
COMPUTATION OF THREE-POINT PROBLEM



Cases 1 and 2			Case 3
P'	128	37 34.7 ✓	P'
P''	29	50 35.5 ✓	P''
A	94	55 27.3 ✓	
Sum	253	23 37.5 ✓	Sum
1/2 Sum	126	41 48.8 ✓	A
S = 180° - 1/2 sum =	53	18 11.2 ✓	A - sum
Log c =	3.486	237 ✓	
Log sin P' =	9.892	781 ✓	
Colog b =	6.113	846 ✓	
Colog sin P'' =	0.303	095 ✓	
Sum = log tan Z =	9.795	959 ✓	
Z =	32	00 36.2 ✓	
Z + 45° =	77	00 36.2 ✓	
Log cot (Z + 45°) =	9.363	016 ✓	
Log tan S =	0.127	673 ✓	
Sum = log tan ε =	9.490	689 ✓ (sign +)	
ε	17	11 54.1 ✓	
S	53	18 11.2 ✓	
(Tan ε+)			(Tan ε-)
S + ε = angle ABP	70	30 05.3 ✓	S - ε = angle ABP
S - ε = angle ACP	36	06 17.1 ✓	S + ε = angle ACP

BPA	29.50-35.5 ✓	APC	128.37-34.7 ✓	PCB	15.07-02.3 ✓
ABP	70.30-05.3 ✓	PCA	36.06-17.1 ✓	CBP	06.24-47.4 ✓
PAB	79.39-19.2 ✓	CAP	15.16-08.2 ✓	BPC	158.28-10.2 ✓
	180.00-00.0 ✓		180.00-00.0 ✓		179.59-59.9 ✓

(For explanation of this form see Special Publication No. 138, pages 191 and 192, or Special Publication No. 145, pages 98-100)

Comp. F.S.T.
gtr

Fourth Order

COMPUTATION OF TRIANGLES

State: VIRGINIA

11-9121

U.S. GOVERNMENT PRINTING OFFICE: 1929

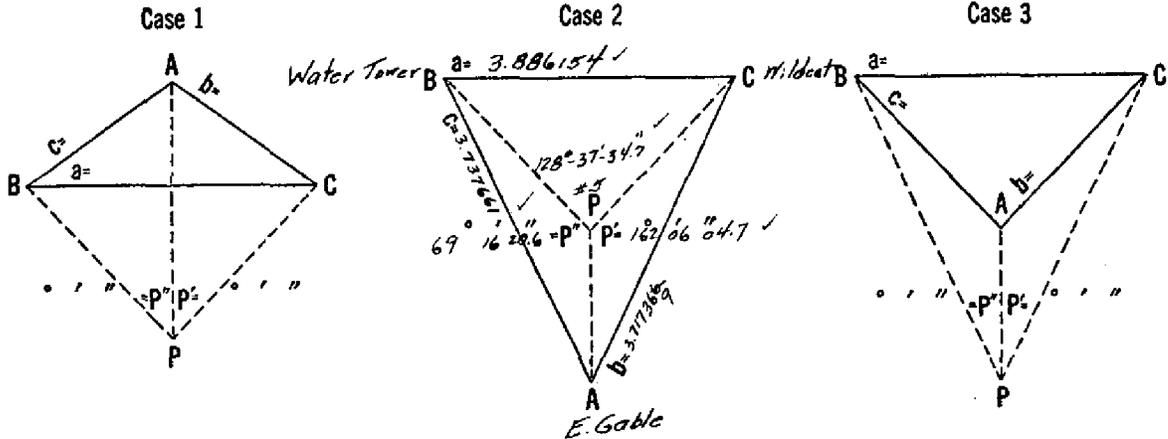
NO.	STATION	OBSERVED ANGLE	CORR'N	SPHER'L ANGLE	SPHER'L EXCESS	PLANE ANGLE AND DISTANCE	LOGARITHM
<i>From fix: Assateague Lt. Ho., Water Tank, Wildcat</i>							
2-3							3.486237 /
1	No. Five	29° 50' 35.5"					0.303095 /
2	Assateague Lt. Ho.	70-30-05.3 /					9.974350 /
3	Chin. Water Tower	79-39-19.2 /					9.992883 /
1-3							3.763682 /
1-2							3.782215 /
2-3							3.886154 /
1	No. Five	128° 37' 34.7"					0.107219 /
2	Chin. Water Tower	15-16-08.2 /					9.420534 /
3	Wildcat, 1909	36-06-17.1 /					9.770309 /
1-3							3.413907 /
1-2							3.763682 /
2-3							3.930551 /
1	No. Five	158° 28' 10.3"					0.435339 /
2	Assateague Lt. Ho.	06-24-47.4 /					9.048043 /
3	Wildcat, 1909	15-07-02.3 /					9.416301 /
1-3							3.413933 /
1-2							3.782191 /
		Adjusted +0.1"					
2-3							
1							
2							
3							
1-3							
1-2							

Do not write in this margin

Copy by Jent
✓ by J.S.T.
Copy by Jent
" " J.S.T.

Fourth Order

COMPUTATION OF THREE-POINT PROBLEM



Cases 1 and 2		Case 3			
P'	162° 06' 04.7"	P'			
P''	69° 16' 20.6"	P''			
A	92° 07' 20.2"				
Sum	323° 29' 45.5"	Sum			
1/2 Sum	161° 44' 52.8"	A			
S = 180° - 1/2 sum =	18° 15' 07.2"	A - sum			
Log c =	3.737661	S = 1/2 (A - sum) =			
Log sin P' =	9.487612				
Colog b =	6.282631				
Colog sin P'' =	0.029061				
Sum = log tan Z =	9.5369685				
Z =	18° 59' 59.7"				
Z + 45° =	63° 59' 59.7"				
Log cot (Z + 45°) =	9.6881857				
Log tan S =	9.518236				
Sum = log tan ε =	9.206423	(sign +)			
ε	9° 08' 15.7"				
S	18° 15' 07.2"				
(Tan ε +)		(Tan ε -)			
S + ε = angle ABP	27° 23' 23.2"	S - ε = angle ABP			
S - ε = angle ACP	09° 06' 51.2"	S + ε = angle ACP			
BPA	69° 16' 20.6"	APC	162° 06' 04.7"	PCB	36° 06' 50.3"
ABP	27° 23' 23.2"	PCA	09° 06' 51.2"	CBP	15° 15' 35.7"
PAB	83° 20' 16.3"	CAP	08° 47' 04.2"	BPC	128° 37' 34.7"

(For explanation of this form see Special Publication No. 138, pages 191 and 192, or Special Publication No. 145, pages 98-100)

Comp by J. J. J.
V " J. J. J.

Fourth Order

COMPUTATION OF TRIANGLES

State: VIRGINIA

11-9121

U. S. GOVERNMENT PRINTING OFFICE: 1928

NO.	STATION	OBSERVED ANGLE	CORR'N	SPHER'L ANGLE	SPHER'L EXCESS	PLANE ANGLE AND DISTANCE	LOGARITHM
2-3							3.787661 ³ ✓
1	No. Five	69° 16' 20.6" ✓					0.029061 ✓
2	East Gable	83- 20- 16.82					9.997057 ✓
3	Chin. Water Tower	27- 23- 23.82					9.662796 ⁷ ✓
1-3							3.783779 ⁶ ✓
1-2							3.429518 ⁹ ✓
2-3							3.886154 ✓
1	No. Five	128° 37' 34.7" ✓					0.107219 ✓
2	Water Tower	15- 15- 35.80					9.420278 ✓
3	W. Idcat, 1909	36- 06- 50.3 ✓					9.770405 ✓
1-3							3.413651 ✓
1-2							3.763778 ✓
2-3							Compt by Gen. ✓ J. S. J.
1							
2							
3							
1-3							
1-2							
2-3							
1							
2							
3							
1-3							
1-2							

Do not write in this margin

Station: Ken

State: Maryland

Chief of party: C. V. H.

Date: 1917

Computed by: O. P. S.

Observer: C. V. H.

Instrument: No. 168

Checked by: W. F. R.

OBSERVED STATION	Observed direction			Eccentric reduction	Sea level reduction	Corrected direction with zero initial			Adjusted direction
	°	'	"			°	'	"	
Chevy	0	00	00.00	-	7.31	0	00	00.00	
Tank west of Δ Dulce	29	03	37.0	-1	09.8	29	02	34.5	
Ken (center), 3.469 meters	176	42							
Forest Glen standpipe	313	24	53.0	+3	01.2	313	28	01.5	
Home	326	31	30.21	+	31.93	326	32	09.45	
Bureau of Standards, wireless pole	352	17	20.8	+	5.7	352	17	33.8	
Reno	357	28	48.63	-	1.16	357	28	54.78	
Reference mark, 16.32 m	358	31	20						

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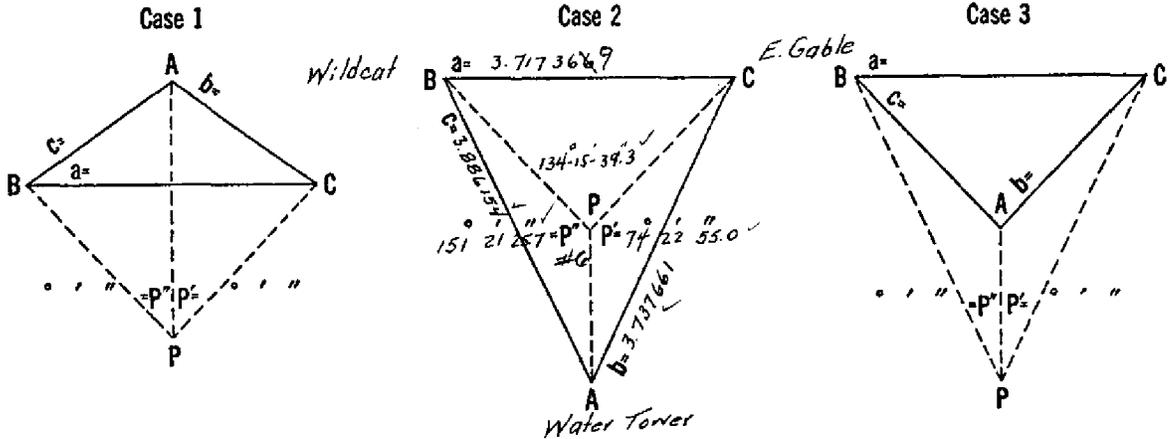
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Fourth Order
COMPUTATION OF THREE-POINT PROBLEM

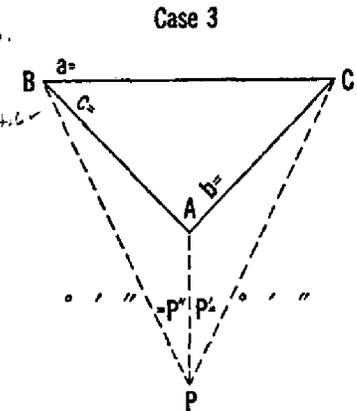
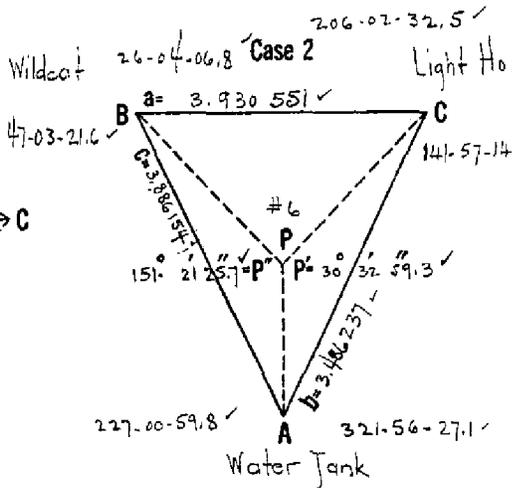
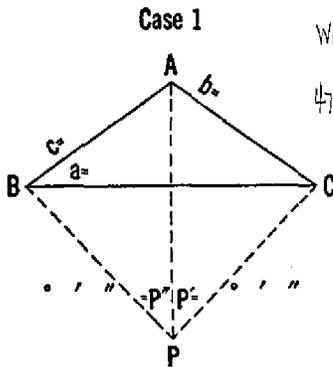


Cases 1 and 2		Case 3			
P'	74°-22'-55.0"	P'			
P''	151°-21'-25.7"	P''			
A	42°-38'-58.2"				
Sum	268°-22'-18.9"	Sum			
1/2 Sum	134°-11'-39.4"	A			
S = 180° - 1/2 sum =	45°-48'-20.6"	A - sum			
		S = 1/2 (A - sum) =			
Log c =	3.886154				
Log sin P' =	9.983661				
Colog b =	6.262339				
Colog sin P'' =	0.319349				
Sum = log tan Z =	0.414503	<i>This is computed as a check on fix: Water Tower, Wildcat, Light House.</i>			
Z =	70°-31'-37.3"				
Z + 45° =	115°-31'-37.3"				
Log cot (Z + 45°) =	9.679023 <i>n</i>				
Log tan S =	0.012216				
Sum = log tan ε =	9.691239	(sign <i>n</i>)			
ε =	26°-09'-33.3"				
S =	45°-48'-20.6"				
(Tan ε+)		(Tan ε-)			
S + ε = angle ABP	19°-38'-47.3"	S - ε = angle ABP			
S - ε = angle ACP	71°-57'-53.9"	S + ε = angle ACP			
BPA	151°-21'-25.7"	APC	74°-22'-55.0"	PCB	20°-09'-26.3"
ABP	19°-38'-47.3"	PCA	71°-57'-53.9"	CBP	25°-34'-54.3"
PAB	08°-59'-47.0"	CAP	33°-39'-11.1"	BPC	134°-15'-39.3"

(For explanation of this form see Special Publication No. 138, pages 191 and 192, or Special Publication No. 145, pages 98-100)

59.9
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✓ J.S.J.

Fourth Order
COMPUTATION OF THREE-POINT PROBLEM



Cases 1 and 2			Case 3
P'	30	32	59.3 ✓
P''	151	21	25.7 ✓
A	94	55	27.3 ✓
Sum	276	49	52.3 ✓
½ Sum	138	24	56.2 ✓

$S = 180^\circ - \frac{1}{2} \text{sum} = 41 \quad 35 \quad 03.8 \checkmark$ $S = \frac{1}{2} (A - \text{sum}) =$

Log c = 3.886 154 ✓
Log sin P' = 9.706 109 ✓
Colog b = 6.513 763 ✓
Colog sin P'' = 0.319 349 ✓

Sum = log tan Z = 10.425 375 ✓

Z = 69 25 05.5 ✓
Z + 45° = 114 25 05.5 ✓

Log cot (Z + 45°) = 9.657 059 ✓
Log tan S = 9.948 097 ✓

Sum = log tan ε = 9.605 156 ✓ (sign -)

ε 21 56 33.4 ✓
S 41 35 03.8 ✓

(Tan ε +)
S + ε = angle ABP
S - ε = angle ACP

(Tan ε -)
S - ε = angle ABP
S + ε = angle ACP

BPA 151-21-25.7 ✓
ABP 19-38-30.4 ✓
PAB 09-00-03.9 ✓

APC 30-32-59.3 ✓
PCA 63-31-37.2 ✓
CAP 85-55-23.5 ✓

PCB 00-33-40.7 ✓
CBP 01-20-44.4 ✓
BPC 178-05-35.0 ✓

180-00-00.0

180-00-00.0

180-00-00.1

(For explanation of this form see Special Publication No. 138, pages 191 and 192, or Special Publication No. 145, pages 98-100)

Comp'd by J.S.T.
✓ by Jem

Fourth Order

COMPUTATION OF TRIANGLES

State: VIRGINIA

11-9121

NO.	STATION	OBSERVED ANGLE	CORR'N	SPHER'L ANGLE	SPHER'L EXCESS	PLANE ANGLE AND DISTANCE	LOGARITHM
		From 3-pt. fix: Water Tank, Wildcat, & Light House					
	2-3						3.486237'
	1 No. Six	30° 32' 59.3'					0.293891'
	2 Assateague Lt. Ho	63- 31 - 37.2'					9.951893'
	3 Chin. Water Tower	85- 55 - 23.5'					9.998900'
	1-3						3.732021'
	1-2						3.779028'
	2-3						3.886154'
	1 No. Six	151° 21' 25.7'					0.319349'
	2 Chin. Water Tower	09- 00 - 03.9'					9.194384'
	3 Wildcat, 1909	19- 38 - 30.4'					9.526518'
	1-3						3.999887'
	1-2						3.732021'
	2-3						
	1						
	2						
	3						
	1-3						
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Fourth Order

COMPUTATION OF TRIANGLES

State: VIRGINIA

11-9121

NO.	STATION	OBSERVED ANGLE	CORR'N	SPHER'L ANGLE	SPHER'L EXCESS	PLANE ANGLE AND DISTANCE	LOGARITHM
	2-3	From 3-pt. fix: Water Tank, Wildcat, E. Gable					3.737661'
	1 No. Six	74° 22' 55.0'					0.016339'
	2 E. Gable, 1902	71-57-53.9'					9.978120'
	3 Chin. Water Tower	33-39-11.1'					9.743638'
	1-3						3.732120'
	1-2						3.497638'
	2-3						3.717368 ⁹
	1 No. Six	134° 15' 39.3 ⁴ '					0.14798 ⁵
	2 Wildcat, 1909	25-34-54.3'					9.635281'
	3 E. Gable, 1902	20-09-36.3 ² '					9.53737 ¹⁴
	1-3						3.49763 ⁵
	1-2						3.399 ⁶⁶⁸ ₇₂₇
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Fourth Order
POSITION COMPUTATION, THIRD-ORDER TRIANGULATION

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		FIRST ANGLE OF TRIANGLE											
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